



National Physical Laboratory

CALCULATION OF UNCERTAINTIES IN STACK MONITORING

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Acknowledgements

- This lecture is based largely on the previous lecture prepared by Dr Andrew Clarke
- It has been updated by Rod Robinson and includes an example based on the CEN/TS 17021 Stationary source emissions - Determination of the mass concentration of sulphur dioxide by instrumental techniques

Overarching :

- **ISO/IEC 98-3:2008 / ENV 13005:1999** – Guide to the expression of uncertainty in measurement (GUM)

<https://www.bipm.org/en/publications/guides/gum.html>

- **BS EN ISO 14956:2002** Air quality - Evaluation of the suitability of a measurement procedure by comparison with a required measurement
- **BS EN ISO 20988: 2007** Air quality – Guidelines for estimating measurement uncertainty (Esp. Annex E dealing with AMS)

Standards for individual SRMs

General guidance

- EURACHEM / CITAC Guide CG 4 : Quantifying Uncertainty in Analytical Measurement

https://www.eurachem.org/images/stories/Guides/pdf/QUAM2012_P1.pdf

- NPL offer some free guides on uncertainties

<https://www.npl.co.uk/resources/gpgs/all-gpgs>

- NPL run some e-learning courses:

<https://training.npl.co.uk/>

Literature - STA

- *“Guidance on assessing measurement uncertainty in stack emissions monitoring”*
2nd Edn 2004 by Jonathan Pullen and Rod Robinson
Source Testing Association QGN001-r1
- Particles by 13284-1 (QGN001-01) but see new standard
BS EN 13284-1 2017
- Example spreadsheets – for most SRMs including flow
BS EN ISO 16911-1:2013

- **Technical Guidance Note M2
Monitoring of stack emissions to air V12, 2017**

Section 4.10 - pages of general guidance relating to measurement uncertainty

Section 6 - a more detailed treatment of the principles and practice of uncertainty calculation.

Section 7 - Table of *maximum permissible measurement uncertainties* covering species of pollutant beyond those in EU standards.

Used in assessing compliance of measurements with ELVs. Uncertainty subtracted from measured value before comparison with ELV.

<https://www.gov.uk/government/publications/m2-monitoring-of-stack-emissions-to-air>

Overall Uncertainties for Standard Reference Methods

Pollutant	BS EN Standard	Uncertainty Requirement
H ₂ O Manual	14790:2017*	±20% of measured value
SO ₂ Manual	14791:2017*	±20% relative at daily ELV
NO _x Chemiluminescence	14792: 2017*	±10% relative at daily ELV
O ₂ Paramagnetic	14789:2017*	±6% of measured value
CO Infra Red	15058:2017*	±6% relative at daily ELV
HCl Manual	1911:2010	±30% relative at daily ELV (for LCP and WID plant)
SO ₂ Instrumental	TS 17021:2017	±15% relative at daily ELV

* or the lowest limit value specified for the plant by the local authorities

O₂ 6% relative or 0.3% absolute.

Note uncertainty requirement is generally expressed as relative to ELV on a dry basis before correction to the oxygen reference

Uncertainties for SRMs

- Overall uncertainties incorporating all possible significant sources of variation
- **Expanded** uncertainties with 95% confidence limits
- H_2O , O_2 relative to the actual measured concentration whilst the rest are relative to the daily Emission Limit Value (ELV)
- Note – must report expanded uncertainty on reported value – but requirement in standard to check requirement is met is before oxygen correction.

General Approach

1. Specify what is being measured and the parameters on which it depends - *model equation*
2. Identify possible sources of uncertainty for each parameter
3. Quantify the component standard uncertainties u i.e.. prepare the **uncertainty budget**
Calculate all component uncertainties in same way – either as percentage (relative) uncertainties or in units of reported value (standard)
Recommend to use units of reported value.

General Approach

4. Determine the combined standard uncertainty of the measured value u_c

Then determine the expanded uncertainty U_c

$$\text{Concentration} = X \pm U_c$$

where U_c is the **overall uncertainty** at a confidence level of 95%.

1. Problem Specification

Manual Methods - gases or particles

Specify the “model equation” relating input quantities to the required concentration:-

Mass Concentration in flue gas

$$= (\text{Mass collected}) \div (\text{Sample gas volume})$$

Mass of particles = (Weight Filter + Particles) – Filter weight
also include washing weight if significant

Mass of Gas = (Solution Concentration) x (Solution Volume)

Sample gas vol = (Meas. Sample gas vol) $(T_{\text{ref}} / T_{\text{act}})$ $(P_{\text{act}} / P_{\text{ref}})$
(at ref. T and P) (at actual T,P)

1. Problem Specification

Manual methods – gases or particles

- Uncertainty of weighing particles
- Uncertainty of chemical analysis of solution
- Uncertainty of measurement of sample gas volume or liquid solution volume
- Uncertainty of meter temperature or pressure
- + Efficiency of sampling bottles in collecting the measurand, leakage and losses in train etc.

1. Problem Specification

- Manual methods –
- Full treatment is included in the newest standards for
 - Particles EN 13284-1, (Annex G)
 - H₂O EN 14790
 - HCl EN 1911
 - SO₂ EN 14791
 - VOC (Speciated) CEN/TS 13649

1. Problem Specification

Instrumental Gas Analysers

- Simple model equation, instrument is calibrated using certified gas

$$\text{Conc} = \text{Instr reading} * \text{factor} + \sum \text{influences}$$

- Factor = calibration factor
 - Influences = whatever may affect reading which is not included in calibration e.g. temp, drift, interfering gases
- Sensitivities of output to factors which may influence it determined experimentally
 - Information from manufacturers and performance characteristics determined during MCERTS testing

2. Identify possible sources of uncertainty for each parameter

Instrumental Gas Analysers

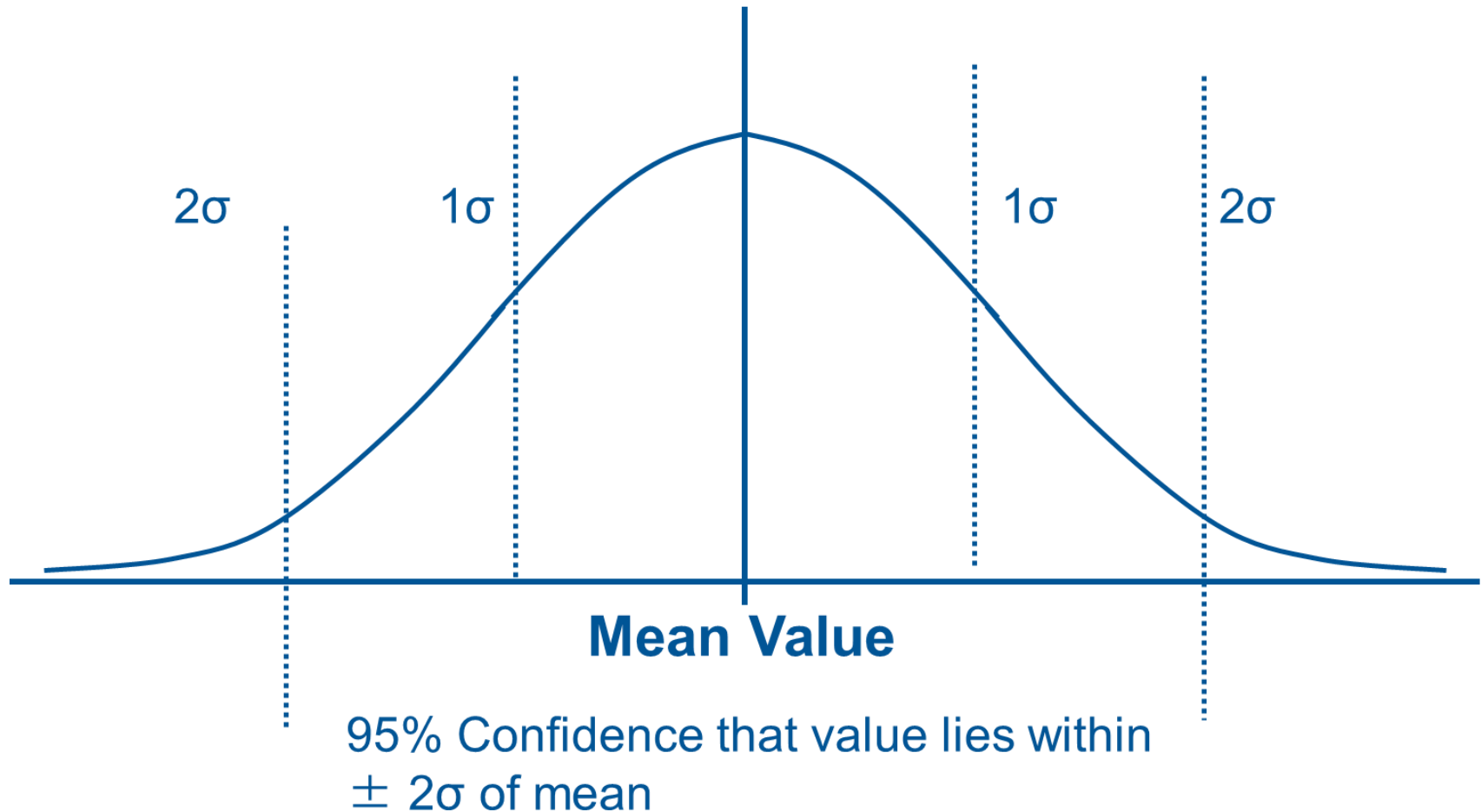
- Lack of fit (linearity)
- Zero drift
- Span drift
- Sensitivity to sample volume flow
- Sensitivity to atmospheric pressure
- Sensitivity to ambient temperature
- Sensitivity to electrical voltage
- Interferences from other gaseous components present in the flue gas
- Repeatability standard deviation in lab at span level*
- Calibration gas
- (*Repeatability standard deviation at zero is not included)

3. Quantify the component standard uncertainties

- **Standard uncertainties u** – those which are obtained from experimental data and thus lead directly to a standard deviation. (“Type A” uncertainties)
- Assuming normal distribution of points around the mean then, with 95% confidence, the uncertainty is ± 2 times the standard deviation.
- The exact factor is 1.96 which is sometimes called the **coverage factor k** .
- When quoting the values, we must be very clear whether we are giving the **standard uncertainty** ($u=1$ SD) or the **expanded uncertainty U** (where $U=k.u$) for a particular degree of confidence such as 95% when $k=2$.

Probability Distributions A

Probability



3. Quantify the component standard uncertainties

Uncertainties from influence quantities

where a parameter of influence has a range of values compared to the value at instrument calibration

e.g. Ambient temp at cal = 298.

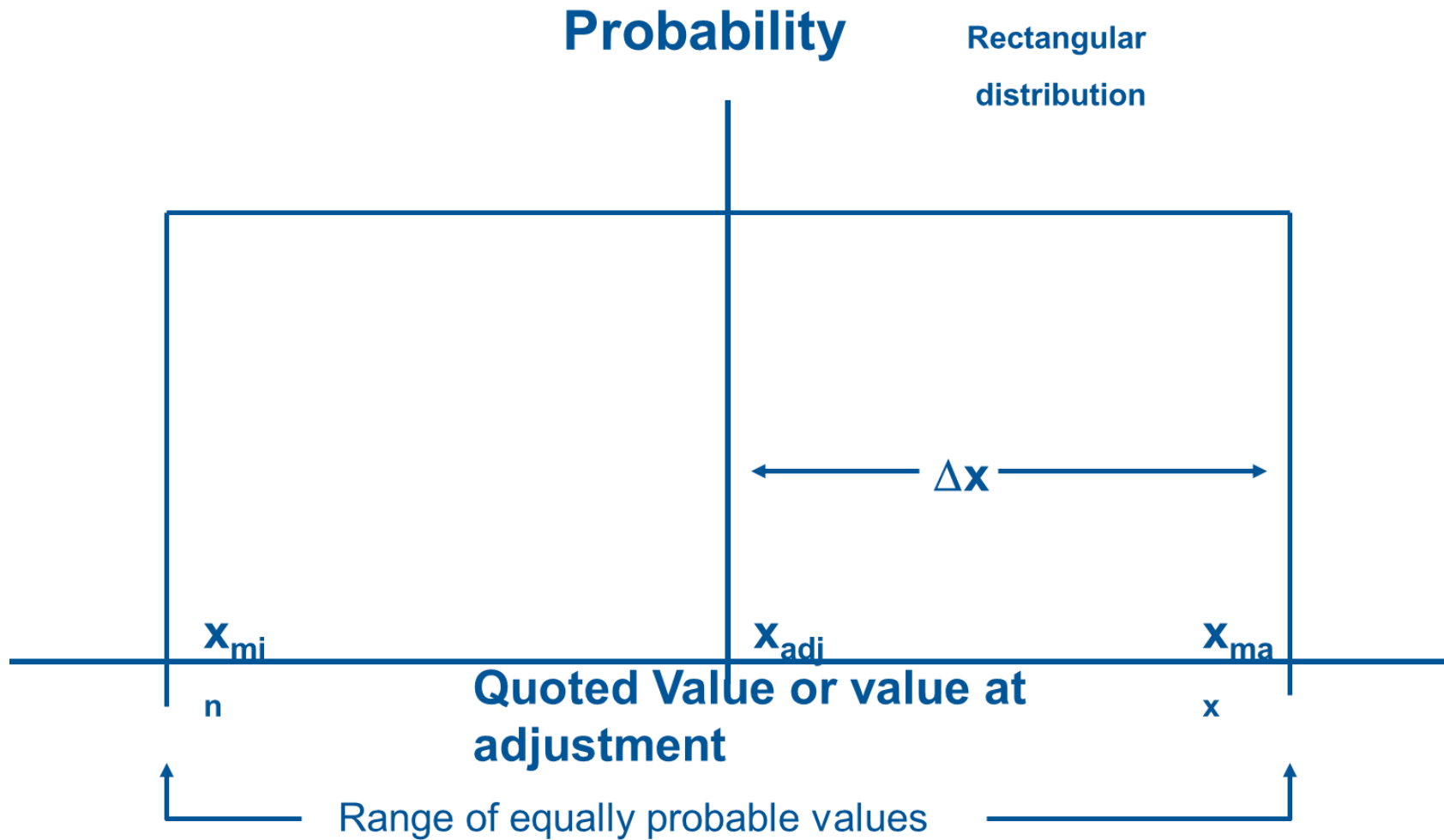
Ambient temp during measurement = 290 to 303.

Other examples

- uncertainty of a physical dimension (e.g. nozzle size)
- uncertainty of voltage during the experimental work

converted to a **standard uncertainty** assuming all values within the range are equally likely (rectangular distribution)

Probability Distributions



Conversion Factors for Type B Uncertainties (see M2)

- . If x_{adj} is halfway between x_{min} and x_{max} then defining

$$\Delta x = (x_{\text{adj}} - x_{\text{min}}) = (x_{\text{max}} - x_{\text{adj}})$$

The standard uncertainty is

$$u_x = \Delta x / (\sqrt{3})$$

- If the value of x_{adj} is offset from the centre of the range then

$$u_x^2 = [(x_{\text{max}} - x_{\text{adj}})^2 + (x_{\text{min}} - x_{\text{adj}})(x_{\text{max}} - x_{\text{adj}}) + (x_{\text{max}} - x_{\text{adj}})^2] / 3$$

Estimating Component Standard Uncertainties

Example

a) Atmospheric pressure variation:

- Measured value 75 mg/m³
- Sensitivity of concentration to atmospheric pressure
0.8% per kPa
- Variation during measurement 99-100 kPa
 $\Delta x = 0.5$
- Standard Uncertainty in concentration units
 $= (0.8/100) \times 75 \times 0.5 / \sqrt{3}$
 $= 0.17 \text{ mg/m}^3$

Estimating Component Standard Uncertainties

Example b) Calibration Gas

An error in the cal gas affects the reported measured concentration directly and proportionately

- Cal gas conc 75mg/m³
- Specified uncertainty 2%
- Type B uncertainty - true concentration 73.5 - 76.5mg/m³
- Standard uncertainty $(2/100) \times 75 / \sqrt{3} = 0.87\text{mg/m}^3$

Rules for Combining Uncertainties

- The mathematical approach is to combine as partial differentials – but there are simple rules for usual cases:
- X obtained by *addition* or *subtraction* – absolute values of component uncertainties combined

$$X = (a \pm u_a) + (b \pm u_b) + (c \pm u_c)$$

$$u_X = \sqrt{u_a^2 + u_b^2 + u_c^2}$$

Rules for Combining Uncertainties

- X obtained by *multiplication* or *division* -
- relative or percentage values of component uncertainties combined

$$X = \frac{(a \pm u_a)(b \pm u_b)}{(c \pm u_c)}$$

$$\frac{u_X}{X} = \sqrt{\left(\left(\frac{u_a}{a} \right)^2 + \left(\frac{u_b}{b} \right)^2 + \left(\frac{u_c}{c} \right)^2 \right)}$$

Rules for Combining Uncertainties

- *Powers and roots* – multiply component uncertainty by value of power (2, 3, 0.5, 0.333, etc)
- Eg $u(x^2) = 2 u(x)$

Neglecting Minor Component Uncertainties.

- When one component uncertainty is much smaller than the others then the smaller one can effectively be neglected
- A factor of four is generally sufficient
- European standards state:
ignore a component uncertainty $<5\%$ of the largest

The Expanded Uncertainty U_c

- Combining all the component standard uncertainties we obtain the *combined uncertainty* u_c
- Multiply by the coverage factor k to obtain the *expanded uncertainty* U_c

$$U_c = k u_c$$

with $k = 2$ for 95% confidence.

The Expanded Uncertainty U_c

- U_c may be calculated in concentration units and then expressed as a percentage by dividing by the ELV
OR the whole calculation may be done in percentages of the ELV.
- Examples in standards are done assuming measured value is at ELV. This is a special case to show performance of the method – most of the time you will calculate the uncertainty at the measured value – and then check this against requirement as a percentage of the ELV

Example: Instrumental SO₂

- Example based on Annex A of CEN TS 17021:2017

(A similar example is give in Annex B of the CO standard BS EN 15058:2017)

- This calculation is based on an ELV of 50 mg.m⁻³

SO₂ site specific conditions

Table 1

Specific conditions	Value/range
Range of analyser	0-26 ppm (0-75 mg/m ₀ 3)
Studied concentration of SO ₂ : limit value of SO ₂ for the site	50 mg/m ₀ 3
Conditions on the field	corresponding to 17 ppm at O _{2,ref}
Sample flow during adjustment	60 l.h ⁻¹
Sample flow variation during monitoring	55 – 65 l.h ⁻¹
Sample pressure during adjustment	100 kPa
Sample pressure variation during monitoring	97.5 – 102.5 kPa
Ambient temperature during adjustment	285 K
Ambient temperature variation during monitoring	283 to 308 K
Voltage during adjustment ^a	110 V
Voltage variation during monitoring	107 – 115.5 V
O ₂ reference concentration : O _{2,ref}	11 % volume
Calibration gas	26 ppm ± 2 %, k = 2
Reading of calibration gas during checking of sampling system	25.7ppm
SO ₂ in N ₂ , without interferent	

Uncertainty Sources

Number Source of uncertainty Assigned symbol	Number Source of uncertainty Assigned symbol	Number Source of uncertainty Assigned symbol
1	Precision of analyser	uread
2	Repeatability standard deviation at span point	ur
3	Lack of fit	ulof
4	Short-term zero drift	ud,z
5	Short-term span drift	ud,s
6	Influence of ambient temperature	uat
7	Influence of electrical voltage	uv
8	Influence of vibration	uvib
9	Influence of sample gas pressure	up
10	Influence of sample gas flow	uf
11	Cross-sensitivity	uint
12	Losses in sample line	uloss
13	Calibration gas	ucal

Symbol	Source of uncertainty	Value	Probability distribution	Divisor d	c_i	$c_i u(x_i)$
u_r	Repeatability standard deviation at span point	0,35 %	normal	1	$\frac{R}{100}$	$c_r \frac{0,35}{d_r}$
u_{lof}	Lack of fit	0,4 %	rectangular	$\sqrt{3}$	$\frac{R}{100}$	$c_{lof} \frac{0,4}{d_{lof}}$
$u_{d,z}$	Zero drift	0,01 %	rectangular	$\sqrt{3}$	$\frac{R}{100}$	$c_{d,z} \frac{0,01}{d_{d,z}}$
$u_{d,s}$	Span drift	0,5 %	rectangular	$\sqrt{3}$	$\frac{R}{100}$	$c_{d,s} \frac{0,5}{d_{d,s}}$
u_{at}	Influence of ambient temperature	0,2 % / 10 K	rectangular	$\sqrt{3}$	$\frac{1}{10} \frac{R}{100}$	$c_{at} \frac{0,2 \sqrt{\frac{(t_{max} - t_{adj})^2}{+(t_{min} - t_{adj})(t_{max} - t_{adj}) + (t_{min} - t_{adj})^2}}}{d_{at}}$
u_v	Influence of electrical voltage	0,12 % / 10 V	rectangular	$\sqrt{3}$	$\frac{1}{10} \frac{R}{100}$	$c_v \frac{0,12 \sqrt{\frac{(v_{max} - v_{adj})^2}{+(v_{min} - v_{adj})(v_{max} - v_{adj}) + (v_{min} - v_{adj})^2}}}{d_v}$
u_{vib}	Influence of vibration	0,4 %	rectangular	$\sqrt{3}$	$\frac{R}{100}$	$c_{vib} \frac{0,4}{d_{vib}}$
u_p	Influence of sample gas pressure	1,0 % / 3 kPa	rectangular	$\sqrt{3}$	$\frac{1}{3} \frac{R}{100}$	$c_p \frac{1,0(P_{max} - P_{adj})}{d_p}$

u_f	Influence of sample gas flow	0,2 % / 10 l.h ⁻¹	rectangular	$\sqrt{3}$	$\frac{1}{10} \frac{R}{100}$	$c_f \frac{0,2(f_{max} - f_{adj})}{d_f}$
u_{int}	Cross-sensitivity	1,4 %	rectangular	$\sqrt{3}$	$\frac{R}{100}$	$c_{int} \frac{1,4}{d_{int}}$
u_{loss}	Losses and leakage in the sampling system	0,3 ppm	rectangular	$\sqrt{3}$	1	$c_{loss} \frac{loss_{max} - loss_{min}}{d_{loss}}$
u_{CRM}	Calibration gas	0,5 ppm, k = 2	normal	2	1	$c_{CRM} \frac{0,5}{d_{CRM}}$
u_c	Combined standard uncertainty		normal			$\sqrt{\sum_{i=1}^N c_i^2 u_i^2(x_i)}$
U_{95}	Expanded uncertainty		t-distribution			$k_{95} u_c$



Symbol	Source of uncertainty	Value	Probability distribution	Divisor d	c_i	$c_i u(x_i)$
u_r	Repeatability standard deviation at span point	0,35 %	normal	1	$\frac{26}{100} = 0,260$	$0,260 \frac{0,35}{1} = 0,091$
u_{lof}	Lack of fit	0,4 %	rectangular	$\sqrt{3}$	$\frac{26}{100} = 0,260$	$0,260 \frac{0,4}{\sqrt{3}} = 0,060$
$u_{d,z}$	Zero drift	0,01 %	rectangular	$\sqrt{3}$	$\frac{26}{100} = 0,260$	$0,260 \frac{0,01}{\sqrt{3}} = 0,002$
$u_{d,s}$	Span drift	0,5 %	rectangular	$\sqrt{3}$	$\frac{26}{100} = 0,260$	$0,260 \frac{0,5}{\sqrt{3}} = 0,075$
u_{at}	Influence of ambient temperature	0,2 % / 10 K	rectangular	$\sqrt{3}$	$\frac{1}{10} \frac{26}{100} = 0,026$	$0,026 \frac{\sqrt{(308-285)^2 + (283-285)(308-285) + (283-285)^2}}{\sqrt{3}} = 0,066$
u_v	Influence of electrical voltage	0,12 % / 10 V	rectangular	$\sqrt{3}$	$\frac{1}{10} \frac{26}{100} = 0,026$	$0,026 \frac{\sqrt{(115,5-110)^2 + (107-110)(115,5-110) + (107-110)^2}}{\sqrt{3}} = 0,009$
u_{vib}	Influence of vibration	0,4 %	rectangular	$\sqrt{3}$	$\frac{26}{100} = 0,260$	$0,260 \frac{0,4}{\sqrt{3}} = 0,060$
u_p	Influence of sample gas pressure	1,0 % / 3 kPa	rectangular	$\sqrt{3}$	$\frac{1}{3} \frac{26}{100} = 0,087$	$0,087 \frac{1,0(102,5-100)}{\sqrt{3}} = 0,125$

u_f	Influence of sample gas flow	0,2 % / 10 l. h ⁻¹	rectangular	$\sqrt{3}$	$\frac{1}{10} \frac{26}{100} = 0,026$	$0,026 \frac{0,2(65 - 60)}{\sqrt{3}} = 0,015$
u_{int}	Cross-sensitivity	1,4 %	rectangular	$\sqrt{3}$	$\frac{26}{100} = 0,260$	$0,260 \frac{1,4}{\sqrt{3}} = 0,210$
u_{loss}	Losses and leakage in the sampling system	0,3 ppm	rectangular	$\sqrt{3}$	1	$1 \frac{0,3}{\sqrt{3}} = 0,173$
u_{CRM}	Calibration gas	0,5 ppm, k = 2	normal	2	1	$1 \frac{0,5}{2} = 0,250$
u_c	Combined standard uncertainty (ppm)		normal			0,419
U_{95}	Expanded uncertainty (ppm)		k = 2			0,838

Calculation of Combined and Expanded Uncertainty

The **combined uncertainty** u_c is obtained as the square root of the sum of the squares of all the component uncertainty u values in the right hand column, converted to mass concentration from which:

$$u_c = 1.20 \text{ mg.m}^{-3}$$

The **Expanded uncertainty** $U_c = 2 \cdot u_c$
 $U_c = \underline{\pm 2.40 \text{ mg.m}^{-3}}$

with level of confidence of 95%.

ELV = 50 mg.m^{-3} so this represents **4.8% of the ELV**

QUESTIONS?

