Stellar Stakeholder meeting, 26-2-2021

C1 WP1: Next generation carbon dioxide isotope ratio gas reference materials

(RUG, NPL, MPI-BGC, AL, UEF, TUBITAK, INRIM, JSI, PTB, LGC, EMPA)

Harro A.J. Meijer, Centre for Isotope Research, University of Groningen (RUG) Work Package Leader





The aim of work package 1 is to **considerably improve** gas reference materials of carbon dioxide that were developed as part of the EMPIR funded SIRS project (16ENV06)....

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...reduce the uncertainties of available atmospheric carbon dioxide standards

First: get pure CO₂ with accurate isotope values, expressed with respect to the internationally accepted scales: VPDB and VSMOW

Then: "dissolve" this CO_2 into CO_2 -free air to create CO_2 in air of which the isotope values are known as well

In parallel: try to realise that isotope ratio values for CO₂ gas will be directly traceable to SI, with sufficient acuracy



First: get pure CO₂ with accurate isotope values, expressed with respect to the internationally accepted scales: VPDB and VSMOW

MPI-BGC, RUG, JSI and UEF will **develop technical capabilities** to perform the carbonate (using IAEA-603) and **phosphoric acid reaction** The reproducibility of the syntheses will be at least 0.01 ‰ and 0.05 ‰ for δ^{13} C- and δ^{18} O-CO₂ respectively. The inter-laboratory compatibility will be tested.



- Synthesis of pure CO₂ from calcium carbonate standards MAR-J1 and IAEA-603 using ARAMIS (Acid Reaction and Air Mixing System)
- Testing different methods to minimize target uncertainties
 - Degassing of H₃PO₄ over different time periods
 - Using different materials for equipment (gold container, glass stirrer etc.)





Preliminary Data MPI-BGC

- Only "good" tries included
- Goal: target uncertainties of 0.05 % for δ^{13} C-CO₂ and 0.1 % for δ^{18} O-CO₂

Name	d 13C [‰]	d 180 [‰]	Offset d13C	Offset d180	Comments
MAR-J1 20202177 - Batch 697	1.976	-1.993	0.019	0.108	82nd try
MAR-J1 20202200 - Batch 698	1.983	-1.984	0.026		Problems with pressure (forgot to grease O-ring), gold container not fully cleaned/wet? Some MAR-J1 powder at edge 7 looked wet
MAR-J1 20202245 - Batch 699	1.951	-2.011	0.006	0.090	0
MAR-J1 20202245 - Batch 699	1.952	-2.016	0.005	0.085	5
MAR-J1 20202256 - Batch 700	1.964	-1.977	0.007	0.124	4
MAR-J1 20202256 - Batch 700	1.961	-1.963	0.004	0.138	8
MAR-J1 20202259 - Batch 701	1.984	-2.007	0.027	0.094	4 different H3PO4
MAR-J1 20202259 - Batch 701	1.989	-2.026	0.032	0.075	5
MAR-J1 20210128 - Batch 703	1.949	-2.127	0.008		new glass stirrer which was stuck for a few hours and thus didn't stirr, usual H3PO4, degassed H3PO4 for a 6 day
MAR-J1 20210128 - Batch 703	1.950	-2.132	0.007	0.031	1 rep ok

Already in target range, newest Batches not measured yet

Next steps: Continue to synthesize 6 MAR-J1 and 4 IAEA-603 samples



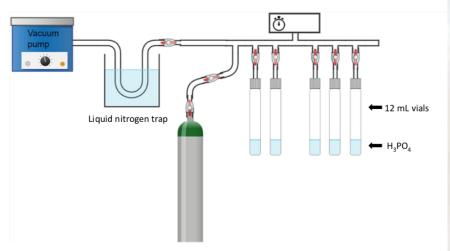
Jožef Stefan Institute Mar-J1 measurements on Europa Scientific 20-20 IRMS with ANCA TG with modification of CaCO₃ - H₃PO₄ gas evolving techniques with objective to use lesser amounts of RMs

Expected values (Brandt t al., 2009)

Determination	δ ¹³ C ‰ (VPDB)	SD (replicates)	δ ¹⁸ Ο ‰ (VPDB	SD
Mar-J1	1.957	0.11	-2.101	0.013

Our preliminary results (carbon)

Determination	δ ¹³ C ‰ (VPDB)	SD				
Mar-J1	2.02	0.02 (n=10)				



N₂ or CO₂ free synthetic air to fill up to atmospheric pressure



experienced with carbonates-phosphoric acid, but corona-related delays. Intercomparisons with MPI-BGC performed in the recent past





wants to develop a system similar to JSI, but corona-related delays Next: "dissolve" the known CO_2 into CO_2 -free air to create CO_2 in air of which the isotope values are known as well

Produce mixtures at an ambient amount fraction (410 μ mol mol⁻¹). CO₂-free air matrix such that the remaining CO₂ has negligible influence. carbon dioxide will be added by using the gravimetric method and also by dynamic dilution

Resulting CO₂ in air calibrated on the JRAS-06 scale

Air Liquide

Empty cylinders with internal treatment

- 26 B10 l cyl prepared and waiting for sending to NPL in the Spanish custom (NPLvalve)

- 20 B05 | and 2 B10 | cyl with DIN-1 or UNI 11144-5 valves for VSL, TUBITAK and INRIM in preparation for Aculife III Megalong treatment

Pure gases N2, O2 & Ar 50 L 200 bar

- 12 cyl N2 + 3 cyl O2 + 1 Cyl Ar sent to NPL Nov 2020
- 14 cyl N2 waiting for sending to NPL in the Spanish custom



Brexit delays!



Pure gases from Air Liquide

N₂ 78.1 % O₂ 20.93 % Ar 0.93 % N₂O 330 ppb	NPL INRIM TUBITAK	410 ppm CO ₂ mixtures to be made by M12 using SIRS pure CO ₂ RMs.
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10 L cylinders from Air Liquide (Aculife – Megalong passivation)

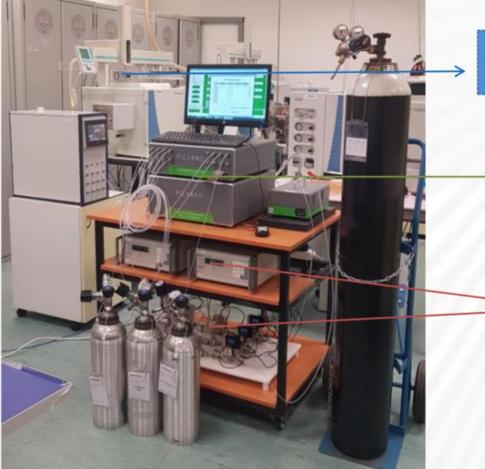
First batch to be sent by end of March 2021

- Cylinders conditioned with 5 bar dry N2 (H2O < 3 ppm), evacuated to < 5 x10⁻⁷ mBar.
- Preparation by gravimetry: N2 78.1 % O2 20.93 % Ar 0.93 % N₂O 330 ppb
 - Validation of composition using existing NPL standards. (GC and CRDS)
- Analysis of residual CO2/CH4/CO/H2O in selected cylinders from each batch
 - Dynamic dilution using existing NPL standards. (CRDS)



Dynamic gas mixture generation and measurement system





IRMS facility (Thermo Finnigan MAT 253 with an autosampler gas injection to GC-IRMS)

CRDS (Picarro G2401) $CO/CO_2/CH_4/H_2O$ Analyzer equipped with 16-Port Distribution Manifold

Dynamic dilution system

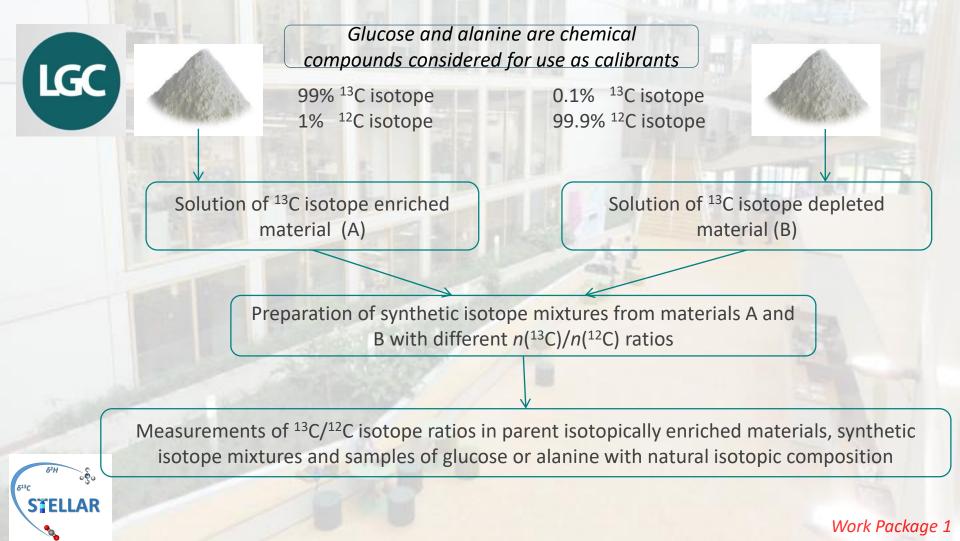
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Already experienced in this technique from the previous project, now for higher accuracy

Work Package 1

In parallel: try to realise that isotope ratio values for CO_2 gas will be directly traceable to SI, with sufficient acuracy

select and purchase suitable compounds (including carbon dioxide gases) enriched in ¹³C and ¹²C isotopes to be used in preparation of calibration mixtures. Chemical and isotopic purity of these compounds will be assessed.



PTB and LGC will set up MS Excel-based spreadsheets for performing all calculations

PB

$\int \frac{m_{\rm A} \times R_{13,\rm A}}{(m_{\rm A} \times M_{12}) - M^{(12}{\rm C}) - M^{(13}{\rm C}) \times R_{13,\rm A}} = \sqrt{M^{(16}{\rm O})} - M^{(17}{\rm O}) \times R_{17,\rm A} - M^{(18}{\rm O}) \times R_{18,\rm A}}$	$\frac{1}{1}$ +]
$\frac{(R_{13,A}+1)\left(\frac{M(^{12}C)}{R_{13,A}+1}+\frac{M(^{13}C)\times R_{13,A}}{R_{13,A}+1}+2\left(\frac{M(^{16}O)}{R_{17,A}+R_{18,A}+1}+\frac{M(^{17}O)\times R_{17,A}}{R_{17,A}+R_{18,A}+1}+\frac{M(^{18}O)\times R_{18,A}}{R_{17,A}+R_{18,A}+1}+\frac{M(^{18}O)\times R_{18,A}}{R_{18,A}+1}+\frac{M(^{18}O)\times R_{18,A}}{R_$	
$0 = K_{45} \times R_{45AB}^{\rm m} - \frac{\left[\frac{M(^{12}{\rm C})}{(R_{13,\rm B}+1)} + \frac{M(^{13}{\rm C}) \times R_{13,\rm B}}{R_{13,\rm B}+1} + 2\left(\frac{M(^{16}{\rm O})}{R_{17,\rm B}+R_{18,\rm B}+1} + \frac{M(^{17}{\rm O}) \times R_{17,\rm B}}{R_{17,\rm B}+R_{1(,\rm B}+1} + \frac{M(^{18}{\rm O}) \times R_{18,\rm B}}{R_{17,\rm B}+R_{18,\rm B}+1}\right]}{m_{\rm A}}\right]}$))
$ \begin{bmatrix} \frac{m_{A}}{(R_{13,A}+1)\left(\frac{M(^{12}C)}{R_{13,A}+1}+\frac{M(^{13}C)\times R_{13,A}}{R_{13,A}+1}+2\left(\frac{M(^{16}O)}{R_{17,A}+R_{18,A}+1}+\frac{M(^{17}O)\times R_{17,A}}{R_{17,A}+R_{18,A}+1}+\frac{M(^{18}O)\times R_{18,A}}{R_{17,A}+R_{18,A}+1}+\frac{M(^{18}O)\times R_{18,A}}{R_{18,A}+1}+\frac{M(^{18}O)\times R_{18,A}}{R_{18,A}+1}+\frac{M(^{18}O)\times R_{18,A}}{R_{18,A}+1}+\frac{M(^{18}O)\times$	$\left(\frac{1}{1}\right)^{+}$
$\boxed{(R_{13,\mathrm{B}}+1)\left(\frac{M(^{12}\mathrm{C})}{R_{13,\mathrm{B}}+1}+\frac{M(^{13}\mathrm{C})\times R_{13,\mathrm{B}}}{R_{13,\mathrm{B}}+1}+2\left(\frac{M(^{16}\mathrm{O})}{R_{17,\mathrm{B}}+R_{18,\mathrm{B}}+1}+\frac{M(^{17}\mathrm{O})\times R_{17,\mathrm{B}}}{R_{17,\mathrm{B}}+R_{18,\mathrm{B}}+1}+\frac{M(^{18}\mathrm{O})\times R_{18,\mathrm{B}}}{R_{17,\mathrm{B}}+R_{18,\mathrm{B}}+1}+\frac{M(^{18}\mathrm{O})\times R_{18,\mathrm{B}}}{R_{17,\mathrm{B}}+R_{18,\mathrm{B}}+1}\right)}$	$\overline{))}$
$ \left[2 \times \left(\begin{array}{c} \frac{m_{\rm A} \times R_{17,\rm A}}{(R_{17,\rm A} + R_{18,\rm A} + 1) \left(\frac{M(^{12}\rm C)}{R_{13,\rm A} + 1} + \frac{M(^{13}\rm C) \times R_{13,\rm A}}{R_{13,\rm A} + 1} + 2 \left(\frac{M(^{16}\rm O)}{R_{17,\rm A} + R_{18,\rm A} + 1} + \frac{M(^{17}\rm O) \times R_{17,\rm A}}{R_{17,\rm A} + R_{18,\rm A} + 1} + \frac{M(^{18}\rm O) \times R_{18,\rm A}}{R_{17,\rm A} + R_{18,\rm A} + 1} \right) \right) + \frac{1}{m_{\rm B} \times R_{17,\rm B}} + \frac{M(^{12}\rm O) \times R_{13,\rm A} + 1}{R_{17,\rm A} + R_{18,\rm A} + 1} + \frac{M(^{18}\rm O) \times R_{18,\rm A}}{R_{17,\rm A} + R_{18,\rm A} + 1} + \frac{M(^{18}\rm O) \times R_{18,\rm A}}{R_{17,\rm A} + R_{18,\rm A} + 1} + \frac{M(^{18}\rm O) \times R_{18,\rm A}}{R_{17,\rm A} + R_{18,\rm A} + 1} + \frac{M(^{18}\rm O) \times R_{18,\rm A}}{R_{17,\rm A} + R_{18,\rm A} + 1} + \frac{M(^{18}\rm O) \times R_{18,\rm A}}{R_{17,\rm A} + R_{18,\rm A} + 1} + \frac{M(^{18}\rm O) \times R_{18,\rm A}}{R_{17,\rm A} + R_{18,\rm A} + 1} + \frac{M(^{18}\rm O) \times R_{18,\rm A}}{R_{17,\rm A} + R_{18,\rm A} + 1} + \frac{M(^{18}\rm O) \times R_{18,\rm A}}{R_{17,\rm A} + R_{18,\rm A} + 1} + \frac{M(^{18}\rm O) \times R_{18,\rm A}}{R_{17,\rm A} + R_{18,\rm A} + 1} + \frac{M(^{18}\rm O) \times R_{18,\rm A}}{R_{17,\rm A} + R_{18,\rm A} + 1} + \frac{M(^{18}\rm O) \times R_{18,\rm A}}{R_{17,\rm A} + R_{18,\rm A} + 1} + \frac{M(^{18}\rm O) \times R_{18,\rm A}}{R_{17,\rm A} + R_{18,\rm A} + 1} + \frac{M(^{18}\rm O) \times R_{18,\rm A}}{R_{17,\rm A} + R_{18,\rm A} + 1} + \frac{M(^{18}\rm O) \times R_{18,\rm A}}{R_{17,\rm A} + R_{18,\rm A} + 1} + \frac{M(^{18}\rm O) \times R_{18,\rm A}}{R_{17,\rm A} + R_{18,\rm A} + 1} + \frac{M(^{18}\rm O) \times R_{18,\rm A}}{R_{17,\rm A} + R_{18,\rm A} + 1} + \frac{M(^{18}\rm O) \times R_{18,\rm A}}{R_{17,\rm A} + R_{18,\rm A} + 1} + \frac{M(^{18}\rm O) \times R_{18,\rm A}}{R_{17,\rm A} + R_{18,\rm A} + 1} + \frac{M(^{18}\rm O) \times R_{18,\rm A}}{R_{17,\rm A} + R_{18,\rm A} + 1} + \frac{M(^{18}\rm O) \times R_{18,\rm A}}{R_{17,\rm A} + R_{18,\rm A} + 1} + \frac{M(^{18}\rm O) \times R_{18,\rm A}}{R_{17,\rm A} + R_{18,\rm A} + 1} + \frac{M(^{18}\rm O) \times R_{18,\rm A}}{R_{17,\rm A} + R_{18,\rm A} + 1} + \frac{M(^{18}\rm O) \times R_{18,\rm A}}{R_{17,\rm A} + R_{18,\rm A} + 1} + \frac{M(^{18}\rm O) \times R_{18,\rm A}}{R_{17,\rm A} + R_{18,\rm A} + 1} + \frac{M(^{18}\rm O) \times R_{18,\rm A}}{R_{17,\rm A} + R_{18,\rm A} + 1} + \frac{M(^{18}\rm O) \times R_{18,\rm A}}{R_{17,\rm A} + R_{18,\rm A} + 1} + \frac{M(^{18}\rm O) \times R_{18,\rm A}}{R_{17,\rm A} + R_{18,\rm A} + 1} + \frac{M(^{18}\rm O) \times R_{18,\rm A}}{R_{17,$	
$\left(\frac{M(^{12}C)}{(R_{17,B}+R_{18,B}+1)\left(\frac{M(^{12}C)}{R_{13,B}+1}+\frac{M(^{13}C)\times R_{13,B}}{R_{13,B}+1}+2\left(\frac{M(^{16}O)}{R_{17,B}+R_{18,B}+1}+\frac{M(^{17}O)\times R_{17,B}}{R_{17,B}+R_{18,B}+1}+\frac{M(^{18}O)\times R_{18,B}}{R_{17,B}+R_{18,B}+1}\right)\right)}$	
$ \left[\begin{array}{c} \frac{m_{\rm A}}{(R_{17,{\rm A}}+R_{18,{\rm A}}+1) \left(\frac{M(^{12}{\rm C})}{R_{13,{\rm A}}+1}+\frac{M(^{13}{\rm C})\times R_{13,{\rm A}}}{R_{13,{\rm A}}+1}+2 \left(\frac{M(^{16}{\rm O})}{R_{17,{\rm A}}+R_{18,{\rm A}}+1}+\frac{M(^{17}{\rm O})\times R_{17,{\rm A}}}{R_{17,{\rm A}}+R_{18,{\rm A}}+1}+\frac{M(^{18}{\rm O})\times R_{18,{\rm A}}}{R_{18,{\rm A}}+1}+\frac{M(^{18}{\rm O})\times R_{$	
$\left(\frac{M(^{12}C)}{(R_{17,B}+R_{18,B}+1)\left(\frac{M(^{12}C)}{R_{13,B}+1}+\frac{M(^{13}C)\times R_{13,B}}{R_{13,B}+1}+2\left(\frac{M(^{16}O)}{R_{17,B}+R_{18,B}+1}+\frac{M(^{17}O)\times R_{17,B}}{R_{17,B}+R_{18,B}+1}+\frac{M(^{18}O)\times R_{18,B}}{R_{17,B}+R_{18,B}+1}\right)\right)$	

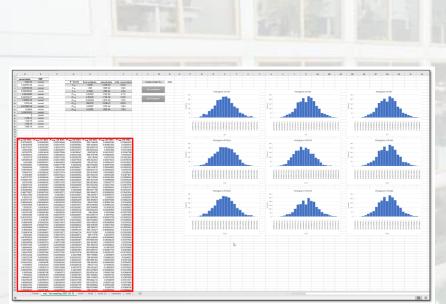
develop an EXCEL tool for solving this system of nine equations...

Work Package 1



quantity	best estimate	uncertainty	PDF						
R 45,A	0.001761091	1.40E-06	normal	×	K-factor	best estimate	uncertainty	relat. uncertainty	number of trails N _{tri} 2000
R 46,A	0.00410269	7.4420 normal triangular			K 45				
R 47,A	5.70E-06	1.2167 rectangula U-shaped			K 46				Start simulation
R 45,8	998.0219381	0.006018894	normal		K 47				startsimulation
R 46,8	19.92759177	0.00038961	normal		R 13,A				
R 47,8	27.42079331	0.000904371	normal		R 17,A				Polt Histograms
R 45,AB	0.985568769	1.0092E-05	normal		R 18,A				Port Histograms
R 46,48	0.025291596	3.07E-06	normal		R 13,5				
R 47,48	0.015216577	4.03769E-06	normal		R 17,8				
mA	1.002	0.00019	normal		R 18,8				
m B	1.002	0.000191382	normal						
M (12C)	12	0	normal						
M (¹³ C)	13.00335484	2.30E-10	normal						
M (¹⁶ O)	15.99491462	1.70E-10	normal						
M (¹⁷ O)	16.99913176	7.00E-10	normal						
M (180)	17.99915961	7.00E-10	normal						





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	quantity	best estimate	uncertainty	PDF		-							
	Rea	0.001761091	1.40E-06	normal		K-factor	best estimate	uncertainty	relat, uncertainty		number	of trails N _{ref}	1
	Reax	0.00410269	7.44207E-08	normal		K 45	1.0010	3.30E-04	0.03%		in the second		
	Reca	5.70E-06	1.21671E-08	normal		K	1.001	1.306-02	1.30%				
	Roca	998.0219381	0.006018894	normal		Kar	0.9949	1.38E-02	1.39%		COLUMN 1		
	Real	19.92759177	0.00038961	normal		RILA	0.001001	7.14E-06	0.71%				÷.,
	8.01	27.42079331	0.000904371	normal		RITA	0.000381	3.76E-06	0.99%		-	in the second se	11
1	Rappa	0.985568769	1.0092E-05	normal	-	RISA	0.002054	2.67E-05	1.30%	_			
				1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1			998.975	3.296-01	0.03%	2			-
	Recis	0.025291596	3.07E-06	normal		Riza							-
_	R 47,48	0.015216577	4.03769E-06	normal		R 11.8	0.00997	1.27E-04	1.28%				
	m,	1.002	0.00019	normal		Roam	0.01360	1.85E-04	1.36%				
	m.	1.002	0.000191382	normal									
	M (⁶² C)	12	0	normal									
	M (¹² C)	13.00335484	2.30E-10	normal									
	M (160)	15.99491462	1.70E-10	normal									
	M(¹² 0)	16.99913176	7.00E-10	normal									
	MI ¹⁸ O	17.99915961	7.00E-10	normal									
	100100												
r	and a second second						2000 2000 2000 2000 2000 2000 2000 200		THE REPORT OF THE REPORT OF THE	1			
L	K _{at} raw data	K _{as} raw data	Kar raw data	R 13.4 raw data	R 12A raw data	R III.A raw data	R 11.8 raw data	R LILE Faw data	R 18.8 rew data				
L	1.00072197	1.004091718	0.997934022	0.001008925	0.000376946	0.002059354	998.7198435	0.010003366	0.013649878				
L	1.001137506	0.999852717	0.993406158	0.001003149	0.000379797	0.002050583	999.1493693	0.009957063	0.013581917				
Ŀ	1.000884093	0.999525182	0.993179287	0.001001987	0.000379175	0.002049892	998.8952879	0.00995636	0.013581726				
ŀ	1.000631097	1.01072612	1.004392161	0.00099631	0.000384017	0.002072877	998.6420939	0.01007064	0.013739018	-			
ŀ	1.001505175	1.027902891	1.023521575	0.001014419	0.000373588	0.002108147	999.509276	0.010233037	0.013987198				
ŀ	1.000925458	0.988473015	0.981309222	0.001002679	0.000381444 0.000377299	0.002027284 0.002084759	998.9217495 999.316768	0.009846264	0.013419331 0.013823869				
ŀ	1.001035268	1.012016293	1.005984929	0.001005545	0.000379405	0.002075534	999.0423021	0.010079425	0.013754784				
ŀ	1.001169572	1.008436157	1.0023884	0.000999747	0.000381822	0.002058158	999.1671431	0.010042437	0.013704023				
ŀ	1.000482891	1.001044177	0.994640664	0.001004956	0.000377796	0.00205299	998.4754856	0.009975784	0.013608502				
ľ	1.00114258	1.00877628	1.001480166	0.0009791	0.000391316	0.002068927	999.1341572	0.010046552	0.013692024				
L	1.000881252	0.996899561	0.989395411	0.0009899	0.000387541	0.002044587	998.8833772	0.009930483	0.013531175				
L	1.00141212	1.019337386	1.014047531	0.001006412	0.000377974	0.002090506	999.4078108	0.010148653	0.013860111				
Ľ	1.000757164	1.019261198	1.014261881	0.001005373	0.000378233	0.002090452	998.7542243	0.010154286	0.013871827				
L	1.00070821	0.99800175	0.991757707	0.001006814	0.00037667	0.002046809	998.7112584	0.009942952	0.013565403				
l	1.000781354	0.998869926	0.992667937	0.001004281	0.000379633	0.002048524	998.7873439	0.009951008	0.013576226				
ŀ	1.000954976	1.013691504	1.007813145	0.001004245	0.000379313	0.002078931	998.9520842	0.010097371	0.013780834				
ŀ	1.001454544 1.000810754	1.007213319 0.995779155	1.000897076 0.988957453	0.001004167	0.000380596	0.002065695	999.4392358 998.8134029	0.010027493 0.009919872	0.013679785 0.013525712				
ŀ	1.000946894	0.98984028	0.982959653	0.001001543	0.000379059	0.00203008	998.9477796	0.009859253	0.013443347				
ŀ	1.001000946	0.99400532	0.986776567	0.000997493	0.000381573	0.002038645	998.9984213	0.009900263	0.013493634				
ľ	1.000299586	0.993178855	0.985427856	0.000992899	0.00038467	0.002036853	998.3010871	0.009899337	0.013484416				
ſ	1.000801873	1.005331704	0.99875172	0.000993928	0.000384045	0.002061768	998.7995706	0.01001511	0.013659411				
L	1.000964109	1.001347434	0.994767767	0.001001931	0.000380645	0.002053591	998.9644613	0.009974065	0.013602939				
E	1.000468022	0.968844231	0.960636833	0.000998289	0.000381303	0.001987024	998.4718161	0.009654744	0.013144509				
	1.001023177	0.004251808	0.097539611	0.000000343	0.000380243	0.002030137	000.0308358	6.0009001103	0.013505209				



Tool is ready, and thoroughly tested by comparing with previously developed Mathematica code. Fully transparant (code included)

Work Package 1

Stellar, WP1, Summary of the initial phase:

Project has started, first developments visible and delivered.

Delays all over the place due to corona, and some also due to the Brexit.

And the pandemic is not over yet, so more delays might happen...

Collaboration between partners runs smoothly, since most partners have collaborated in the previous project. Being accustomed to on-line meetings and workshops is an advantage.

Still, 9 months report is expected to be full of missed deadlines (typical delay is 3-6 months for most activities)

Thank you for your attention

